TALLINNA TEHNIKAÜLIKOOL Elektrotehnika instituut

ATV70LT

Ruslan Kevorkov

RAKETI MOODULI ELEKTROONIKA ARENDAMINE: REGISTER TRANSFER LEVEL DISAIN JA VALIDEERIMINE

Sounding ocket experiment: Register Transfer Level design and validation

Magistritöö

Instituudi direktor	r prof. Tõnu Lehtla
Juhendaja	prof. Valery Vodovozov
Lõpetaja	Ruslan Kevorkov

Tallinn 2014

DECLARATION

I hereby declare that this diploma thesis is entirely the result of my own work and I have faithfully and properly cited all information sources used in the thesis.

Date

Signature

.....

.....

ATV70LT

Raketi mooduli elektroonika arendamine: RTL disain ja valideerimine

Ruslan Kevorkov, üliõpilaskood 111772AAAMM, september 2014. – 87 lk.

TALLINNA TEHNIKAÜLIKOOL

Energeetikateaduskond

Elektrotehnika instituut, elektriajamite ja elektrivarustuse õppetool

Töö juhendaja: professor Valery Vodovozov

Võtmesõnad: ISAAC, sounding rocket, RMU, RTL design, communication, ejection, rocket experiment, validation

Referaat:

Infrapuna spektroskoopia atmosfääri koosseisu analüüsimiseks (ISAAC) on eksperimentaalne moodul, mille arendamisega on tegelenud KTH (Royal Institute of Technology, Stockholm, Rootsi) õpilased. Antud moodul koosneb raketile paigaldatava moodulist (ingl. k. Rocket Mounted Unit, RMU) ja kahest vabalangevast katseseadmest (Free-Falling Unit, FFU). Eksperimendi peamiseks eesmärgiks on katseliselt demonstreerida võimet ühe FFU jälgida teist ning teostada mõõtmisi koostöös.

Käesolev magistritöö hõlmab väljaheitmise süsteemi arendamist ja elluviimist ning reaalajas saadud andmete töötlemist ja salvestamist. Käesoleva lõputöö peaeesmärgiks on tagada õigeaegset vabalangevate moodulite väljalaskmist ning korrektseid operaatorile edastatud ja salvestatud andmeid lennujärgneva analüüsi jaoks. Väljaheitmise kontroll ja side on teostatud programmeeritava ventiilmaatriksi (Field-Programmable Gate Array, FPGA) abil, kasutades VHDL riistvara kirjelduse keelt. Hiljuti väljatöötatud riist- ja tarkvara valideerimise ja lennuanalüüsi tulemused on ka esitatud käesolevas aruandes. ISAAC mooduli lennutati 29. mail Esrange polügoonilt REXUS15 raketi pardal.

ATV70LT

Sounding rocket experiment electronics: RTL design and validation

Ruslan Kevorkov, student code 111772AAAMM, September 2014. – 87 pages

TALLINN UNIVERSITY OF TECHNOLOGY * Faculty of Power Engineering

Department of Electrical Engineering

Chair of Electrical Drives and Electricity Supply

Tutor of the work: professor Valery Vodovozov

Key words: ISAAC, sounding rocket, RMU, RTL design, communication, ejection, rocket experiment, validation

Summary:

The Infrared Spectroscopy to Analyse the middle Atmosphere Composition (ISAAC) is an experimental module designed by KTH (Kungliga Tekniska Högskolan, Stockholm, Sweden) students. It consists of a Rocket Mounted Unit (RMU) and two Free-Falling Units (FFU) carried inside. The main objective of the experiment is to demonstrate ability of one FFU to track the other and to carry out measurements in cooperation.

This Master's thesis covers the development and implementation of the ejection system as well as data acquisition for the ISAAC experiment to have well-timed ejection of the FFUs and data for a post-flight analysis. Ejection control and communication is implemented in a Field-Programmable Gate Array (FPGA) using VHDL hardware description language. Newly developed firmware verification and the post-flight analysis results are also presented in the report.

The ISAAC experiment was launched on May 29 from Esrange, Kiruna onboard the REXUS15 rocket.

ATV70LT

Elektronik för raketmonterad experimentmodul: RTL konstruktion och validering

Ruslan Kevorkov, personnummer 111772AAAMM, September 2014. – 87 sidor.

Tallinns Tekniska Universitet * Ingenjörsteknik inom kraftteknik

Avdelningen för Elektroteknisk ingenjörskonst

Ordförande inom Elektro driv och utbud.

Handledare: professor Valery Vodovozov

Nyckelord: ISAAC, sounding rocket, RMU, RTL design, communication, ejection, rocket experiment, validation

Sammanfattning:

ISAAC (Infrared Spectroscopy to Analyse the Middle Atmosphere Composition) är en raketmonterad experimentmodul designad av studenter på KTH. Modulen består av en raketmonterad modul benämnd RMU (Rocket Mounted Module), i vilken två mindre fritt fallande enheter benämnda FFU (Free Falling Units) sitter monterade. Huvudmålet med experimentet är att demonstrera förmågan för den ena FFU:n att spåra den andra FFU:n samt förmågan att genomföra koordinerade mätningar.

Detta examensarbete behandlar utvecklandet och implementationen av utskjutningssystemet samt datainsamlingen för ISAAC-experimentet. Dessa delar görs för att kunna genomföra utskjutningen vid en lämplig tidpunkt samt få data till efterbehandling. Utskjutningskontroll samt kommunikation är implementerade i en FPGA (Field Programmable Gate Array) i det hårdvarubeskrivande språket VHDL (VHSIC (Very High Speed Integrated Circuit) Hardware Description Language). Verifikation av nyutvecklad inbyggd programvara samt analysresultat av data från uppskjutningen presenteras också.

Uppskjutningen av ISAAC-experimentet skedde den 29:e maj 2014 från rymdbasen Esrange i Kiruna ombord på raketen REXUS15.

Contents

TASK E	DEFIN	ITION	13
Chapter	1	Introduction	15
1.1	Back	ground	15
1.2	Meth	od	16
1.3	Delin	nitation	17
1.4	Goal	and public welfare	17
1.5	Outlin	ne	17
Chapter	2	RMU system	18
2.1	FPGA	A	19
2.2	Comr	munication	19
2.3	Data	acquisition	20
2.4	Came	era	21
2.5	Ejecti	ion system	22
Chapter	3	RMU development	24
3.1	Sun s	ensors	24
3.2	Ejecti	ion algorithm	26
3.2	.1 I	Data receiving processes	27
3.2	.2 Т	۲iming۲	27
3.2	.3 S	Sun sensors data handling process	28
3.2	.4 0	Gyroscope data handling process	32
3.2	.5 E	Ejection activation process	33
3.2	.6 E	Ejection timeout process	34
3.3	Comr	munication	35

3.3.1	RMU communication	
3.3.2	General FFU communication	
3.3.3	RxSU communication	
3.3.4	GUI	
Chapter 4	RMU verification	
4.1 Co	ommunication	
4.2 Ca	mera	
4.3 Ej	ection algorithm	
4.3.1	Division	
4.3.2	Angular rate sensor readings	
4.3.3	Sun sensors readings	
4.3.4	Sun sensors data handling	
4.3.5	Arming procedure	
4.3.6	Ejection timeout	
4.3.7	Ejection activation process	
4.4 Er	vironmental tests	
4.4.1	Vacuum test	
4.4.2	Thermal test	
Chapter 5	Post-flight analysis	
Chapter 6	Discussion and future work	
Chapter 7	Conclusion	
Chapter 8	Arutlus	
Chapter 9	Kokkuvõte	
Bibliograph	ıy	
Appendixes	5	71

Appendix A:	Ejection algorithm	71
Appendix B:	Data_sender	78
Appendix C:	FFU Comm switches	83
Appendix D:	RxSU Comm switch	85

LIST OF FIGURES

Figure 2-1 RMU electrical system [4, p. 67]	
Figure 2-2 Downlink protocol example	20
Figure 2-3 Housekeeping (left) and Ejection (right) ADCs electrical schematics	
Figure 2-4 Desired ejection direction [4, p.7]	22
Figure 2-5 Ejection system power driver	
Figure 3-1 Sun sensor PCB	
Figure 3-2 Electrical schematic for sun sensor PCB	
Figure 3-3 Ejection algorithm block diagram	
Figure 3-4 Sun sensors readings separately	
Figure 3-5 Sun sensors readings	30
Figure 3-6 Sum of readings	30
Figure 3-7 Sun sensors data handling finite state machine	
Figure 3-8 Gyroscope data processing finite state machine	
Figure 3-9 Ejection activation process finite state machine	
Figure 3-10 Data_sender: interaction of internal processes	
Figure 3-11 Ground station GUI	41
Figure 4-1 Uplink and downlink test	43
Figure 4-2 Log file	43
Figure 4-3 Camera signals	44
Figure 4-4 Division block simulation	45
Figure 4-5 Gyroscope data	46
Figure 4-6 Sun sensor data	47
Figure 4-7 Maximum light intensity identification	48
Figure 4-8 Ejection arm signal	49
Figure 4-9 Timeout signal	50
Figure 4-10 Ejection activation algorithm	51
Figure 4-11 Vacuum chamber	52
Figure 4-12 RMU power cable for vacuum test	52
Figure 4-13 Output voltage under vacuum condition	53
Figure 4-14 Heat influence on voltage	54

Figure 4-15 Cold influence on voltage	55
Figure 5-1 Angular velocity of the rocket	57
Figure 5-2 Accelerometer data	57
Figure 5-3 Sun sensors and gyro behavior during the flight	58
Figure 5-4 Camera signals	58
Figure 5-5 Housekeeping data	59
Figure 5-6 Sun sensors readings during the ejection moment	60
Figure 5-7 Example of ejection signal	60
Figure 5-8 Ejection video frame 27224	61
Figure 5-9 Ejection video frame 27243	62

LIST OF TABLES

Table 2-1 Umbilical connector pinout	20
Table 3-1 Global time vector	28
Table 3-2 Division example	33
Table 3-3 Real-time message structure	36
Table 3-4 Time vector structure	36
Table 3-5 "Time within a second" vector	36
Table 3-6 Status vector structure	37
Table 3-7 Housekeeping data packet 1	39
Table 3-8 Housekeeping data packet 2	39
Table 3-9 Real-time message example	39

TALLINN UNIVERSITY OF TECHNOLOGY Department of Electrical Engineering

APPROVED

Prof. T. Lehtla.....

TASK DEFINITION

Ruslan Kevorkov, student code 111772AAAMM

Thesis topic: Sounding rocket experiment electronics: RTL design and validation

<u>Task</u>: To developed and verify electronics for the Rocket Mounted Unit including FPGA firmware and provide a successful launch.

Prestudy:

- 1. Students Experiment Documentation (SED)
- 2. Previously conducted researches and BSc theses

Problem description:

- Solder and troubleshoot a Rocket Mounted Unit (RMU) and sun sensors
- Develop ejection algorithm
- Develop firmware for communication with a ground station operator
- Single block and complete system verification
- Ensure a successful rocket launch
- Post-flight analysis

Current thesis must be presented in English with two additional abstract chapters in Estonian and Swedish. The report must be handed in by 01.09.2014.

Supervisor:

MSc thesis student:

Prof. V. Vodovozov

R. Kevorkov

LIST OF ABBREVIATIONS

ADC	Analogue-to-Digital Converter
CU	Common Unit
DLR	German Aerospace Center
DMM	Digital MultiMeter
Esrange	European Space and Sounding Rocket Range
FFU	Free-Falling Unit
FPGA	Field-Programmable Gate Array
GUI	Graphical User Interface
IR	Infrared
ISAAC	Infrared Spectroscopy to Analyse the middle Atmosphere Composition
LSB	Least significant bit
PCB	Printed Circuit Board
REXUS	Rocket Experiments for University Students
RMU	Rocket Mounted Unit
RTL	Register Transfer Level
RXSM	REXUS Service Module
RxSU	Receiver Specific Unit
SED	Student Experiment Document
SNSB	Swedish National Space Board
SOC	System-on-Chip
SU	Specific Unit
TxSU	Transmitter Specific Unit

1.1 Background

Every year up to eight different teams of students from European universities get an opportunity to take part in Rocket Experiments for University Students (REXUS) program initiated by bilateral cooperation of Swedish National Space Board (SNSB) and German Aerospace Center (DLR). Prospective engineers work on complex mechanical and electrical systems in order to apply earned knowledge, gain skills and conduct successful scientific space experiments [1].

ISAAC (Infrared Spectroscopy to Analyse the middle Atmosphere Composition) is an experimental module designed by KTH students. The main intention for the team was to design, construct and demonstrate a system with two autonomous Free-Falling Units (FFUs), carried inside the Rocket Mounted Unit (RMU), where one FFU can track the other after ejection from the sounding rocket. Each of them consists of a Common Unit (CU), which is inherited from the MUSCAT [2] and the RAIN [3] experiments, and a Specific Unit (SU). The concept of tracking lies in capability of Receiver Specific Unit (RxSU) to fix its position relatively to Transmitter Specific Unit (TxSU) and keep the last within a narrow field of view. Establishing of in a way connection between units makes it reasonable to conduct a scientific experiment. As the secondary objective, definition of profile of carbon dioxide (CO₂) concentration in the middle atmosphere using infrared (IR) spectroscopy method is declared [4].

The ISAAC experiment can be split into six different subsystems from the electronic point of view. The electronics on-board the RMU powers the whole experiment as well as provides communication with FFUs through ground station and schedules ejection. CU is responsible for localization, landing and flight trajectory logging for further reconstruction. Smooth and safe landing is ensured by a parachute deployment system. After the parachute deploys at the altitude of around 6 km, localization system activates the transmission of corresponding FFU GPS coordinates. Constant experiment positioning is essential for recovery. General purpose

of the TxSU is light emission for reaching both experiment goals. It has 20 high power LED sources and eight IR lamps around the periphery. The RxSU, in turn, is divided into a power system and two independent parts, namely the tracking system and the IR spectroscopy system. The power system has six DC/DC converters that provide power for the whole RxSU module. The tracking system gathers and processes data from angular rate sensor, sun sensors and CMOS camera to command two stepper motors. The IR spectroscopy system controls thermoelectric coolers and saves digitalized infrared sensors data to memory for post-flight analysis [4].

The ISAAC was declared as a unique experiment with its controlled ejection and objectives that expect a collaboration of two independent FFUs. However, due to inability to ensure safe flight as well as full operation of the FFUs, a decision to scope down the objectives of the experiment was made in April 2014. The ejection system test was declared as the new goal of the experiment. The rocket was launched on May 29 from Esrange, Kiruna and all objectives of the current thesis work were successfully reached. According to the post-flight analysis based on real-time communication packets, the FFUs were ejected in the correct time window.

1.2 Method

The method followed in the degree project is applied [5]. The research is based on solving practical problems.

In order to get the whole picture of the experiment, Student Experiment Document (SED) and previously conducted researches were studied during first two weeks. Next week after the prestudy period were assigned for software examination and preparation for off-site testing. On week 6 and week 11, the author was involved in bench test and payload integration test in Germany. The last 2 weeks were reserved for the launch campaign in Esrange. All the remaining time the author was focused on practical part and report writing.

1.3 Delimitation

Since there are only 20 weeks allocated for degree project, the author was focused only on the RMU system. FFUs are not a part of discussion in this Master's thesis.

1.4 Goal and public welfare

The goal of the degree project is to develop and verify electronics for the RMU and ensure a successful launch campaign that implies well-timed ejection of the FFUs and data collection for post-processing.

Other KTH teams in later projects will reuse some of the unique parts of the ISAAC experiment or use them as starting points.

1.5 Outline

Logic structure of the report lies in consistent description of the conducted research. It starts with broad overview of the system under research and finishes with a discussion of obtained results and suggestions for future work.

Chapter 2 describes the RMU system and its requirements.

Chapter 3 is dedicated to development part of the RMU system.

Verification phase is described in details in Chapter 4.

Chapter 5 is devoted to post-flight analysis.

In Chapter 6, the conducted work is discussed, bringing suggestions for future work.

Chapter 7 concludes the report.

Chapter 8 and Chapter 9 are dedicated to discussion and conclusion in Estonian..

The RMU is a mechanical module fixed on the rocket. From the electrical point of view, it is an intermediate unit between the rocket and the FFUs, which are carried inside. The electronics on board solves several very important tasks, namely communication, battery charging, data acquisition and ejection's "brain". Although the unit is mostly inherited from previous experiments, radical change in FFUs ejection principle appears in the ISAAC. A block diagram of RMU electrical system is show in Figure 2-1.



Figure 2-1 RMU electrical system [4, p. 67]

The RMU electronics can be divided into 6 different blocks: data acquisition system, ejection system, power system, camera, communication and umbilical communication. The ejection system is responsible for cutting cables using a pyrocutter. The power for the cutter is provided by the REXUS Service Module (RXSM). A driver and an ejection control system ensure a possibility to control ejection time. The data acquisition system is based on a thermal sensor, sun sensors and an angular rate sensor. Readings of these sensors are processed by the FPGA both for housekeeping and ejection control. The umbilical communication allows to control the FFUs while they are inside the RMU. The camera is in charge of ejection video recording. The communication system allows to monitor and control the experiment from a

ground station using downlink and uplink. The power system supplies the whole RMU board as well as charges batteries in the FFUs.

Electrical schematics and a PCB layout was developed by a team of SOC students that the author was part of.

2.1 FPGA

The RMU contains an FPGA that allows the above-mentioned functionality to be implemented. Actel Proasic3 A3P250 is chosen due to its low power consumption, high performance and enough high capacity. It has 250 000 gates, and 3.3V and 1.5V as supply voltage [6]. FPGA is programmed through integrated JTAG interface in Microsemi Libero IDE software using VHDL hardware description language.

The RMU FPGA is in charge of data processing, camera control, ejection scheduling, communication with the FFUs as well as communication with a ground station in real-time mode.

2.2 Communication

Communication in the RMU allows sending commands from a ground station to the FFUs through RXSM. All incoming and outgoing messages are processed in the FPGA and then redirected to FFUs if it is needed.

Communication protocol used in the experiment is RS-422. While the rocket is on the ground, RXSM provides the ground station operator with 38.4 Kbit/s both uplink and downlink, however after liftoff only downlink is available. The example of downlink data structure is shown in Figure 2-2, where SYNC1 and SYNC2 are synchronization bits, MSGID is a message ID, MCNT is a current message number. CSM and CRC are checksum and cyclic redundancy check bits, respectively.



Figure 2-2 Downlink protocol *example*

Each FFU has two independent umbilical connectors: one is for SU and the other is for CU. The pinout of the umbilical connector is shown in Table 2-1.

Pin №	Pin name	Function		
1	ROCKET_PIN	FFU state control (sleep/mission mode)		
2	TX	Transmitting channel to RMU		
3	RX	Receiving channel from RMU		
4	CHARGE	Battery charging		
5	GND	Common ground		

Table 2-1 Umbilical connector pinout

The RMU continuously provides a ground station operator with real-time data. Communication is essential for pre-flight preparations and post-flight analysis. All flash memories have to be erased and rewound; ejection algorithm execution starts only after manual arming. For the post-flight analysis, communication is the only way to receive stored data from flash memory.

2.3 Data acquisition

Data acquisition system in the ISAAC RMU consists of a temperature sensor, three sun sensors and an angular rate sensor. The last two provide ejection algorithm implemented in the FPGA with necessary input data.

The angular rate sensor L3G4200D is a low-power three-axis gyroscope. It is ultra-stable device with digital output and built-in I^2C/SPI communication interfaces. [7]

The sun sensors are SLSD-71N6 planar photodiodes mounted on the skin of the rocket [8]. The distance between three sensors corresponds to 30° angle.

Output of analogue thermal and sun sensors is digitalized with 12-bit MAX11617 analogueto-digital converter (ADC) with 2.048 V internal reference voltage [9]. The RMU has two identical ADCs: housekeeping and ejection. The housekeeping one digitalizes voltage levels and current consumed by the FFUs as well as temperature inside the RMU module. The second ADC digitalizes outputs of sun sensors. Both ADCs are shown on Figure 2-3.



Figure 2-3 Housekeeping (left) and Ejection (right) ADCs electrical schematics

2.4 Camera

The whole flight is recorded with a HD GoPro Hero3 camera. The video will be used later in post-processing to verify the FFUs ejection time and direction relatively to the Sun. Recording function is manually activated by a ground station operator at time t-150s and deactivated automatically at time t+510s, where t is the time of the rocket liftoff. The video will be stored on 32GB microSD card. The RMU camera is mounted on the skin of the rocket inside the module and looks out through a hole. [4]

The camera itself is inherited from the MUSCAT experiment. The battery has been removed and electrical power is provided by the RMU. Moreover, it is fully controlled by the FPGA.

2.5 Ejection system

In this project, presence of voltage in power supply line for pyrocutter is not the only necessary and sufficient condition for ejection of modules. The ejection system can be divided into two major parts: an ejection algorithm and a power driver. The algorithm is being constantly executed producing output after manual arming of the system. The idea of controlled ejection lies in continuous position tracking relatively to the Sun and calculation of a proper instant of time to eject the FFUs. In order to avoid sun influence on the FFU tracking ability, they shall be ejected perpendicularly to the Sun position with allowable deviation of $\pm 20^{\circ}$. Top and side view of the desired ejection is shown in Figure 2-4.



Figure 2-4 Desired ejection direction [4, p.7]

The ejection system is controlled by the RMU and has independent power line from the rocket, which is activated by a flight operator at time t + 90 s, where t is the time of liftoff. The power driver represents an electrical switch that consists of two MOSFET transistors. Electrical schematic of the power driver is shown in Figure 2-5.



Figure 2-5 Ejection system power driver

Gates of N-channel SIPMOS BSP318S are connected to the FPGA output pins. The chosen transistors provide enough current (over 1.2 A) to a pyrocutter with V_{GS} voltage of 3V at high temperatures [10]. The pyrocutter has 1.2 Ω resistance [11] and it is connected in series with high power 10 Ω resistor in order to limit current.

The complexity of the multitasking PCB demands different approaches. The design flow of the electronic system on board the RMU includes both hardware and firmware development.

The RMU hardware consists of four PCBs, where three of them are located on the rocket skin with photodiodes mounted on their surfaces. The main RMU board has 291 components, excluding wires and connectors. Careful soldering is very important for tiny components' operation under space conditions. All components, except angular rate sensor, were soldered manually in KTH SPP students lab. The gyroscope package requires BGA soldering technique and therefore it was mounted by the PCB manufacturer.

3.1 Sun sensors

In order to calculate relative position of the Sun, sun sensors are used. They provide the FPGA with real-time illumination intensity. Figure 3-1 shows top and bottom view of a soldered PCB.



Figure 3-1 Sun sensor PCB

Current, generated by SLSD-71N6 planar photodiode, changes its value proportionally to light density, what in turn changes voltage drop across a resistor. Before sending analogue voltage to ADC, it is being amplified. Figure 3-2 shows the schematic for light to voltage conversion.



Figure 3-2 Electrical schematic for sun sensor PCB

For signal amplification, LM7321 dual-rail operational amplifier is used [13]. +3.3V and - 3.3V supply voltages are provided by the RMU.

Optimal gain should match sun sensor output voltage to the ADC range. The internal reference voltage of the ADC is 2.048 V, which limits the gain. Sun sensor output voltage higher than the ADC reference will saturate it. Applying equation (1) below [12], the optimal gain value of 3.5 is obtained, which is further verified empirically.

$$A_V = 1 + \frac{R_f}{R_g} \quad (1), \text{ where }$$

$$\begin{split} R_f &- \text{feedback resistor } [\Omega] \\ R_g &- \text{gain set resistor } [\Omega] \\ A_v &- \text{operational amplifier gain} \end{split}$$

Sun sensor gain testing was done in sunny and serene day within the precincts of the KTH Campus. All three independent PCBs were powered with batteries and output voltage was measured with digital multimeter (DMM). The maximum indication was 1.1 V, what gives us approximately 1V safety margin.

3.2 Ejection algorithm

Ejection control is one of unique features of the ISAAC. Perpendicular to the Sun position ejection requires continuous data processing in real-time mode. Several approaches of implementation were investigated and analyzed.

Approach 1: In this method, the only source of information are sun sensors. Searching for maximum intensity values, the Sun direction can be easily found. Moreover, observation of more than one rotation allows to determine rotation frequency of the rocket. This method uses fewer sources of data; however, the complexity of firmware code is higher due to necessity of implementation of parallel division. The FPGA space is limited with 250 000 gates and this is the reason why parallel division of two variables cannot be implemented in the RMU. Besides that, requirements fulfilment cannot be guaranteed because only approximate values can be found. The allowable maximum value of deviation is $\pm 20^{\circ}$.

Approach 2: In this method, both light intensity and angular speed are processed from independent sources. The implementation is much easier, occupies less than 50% of FPGA space and results in calculations that are more precise. Division is used to process angular velocity, which do not require high processing speed and therefore can be implemented using sequential division. This method is chosen to be implemented in the final version of the firmware.

The ejection algorithm consists of seven concurrent processes: sun sensors data receiving, gyroscope data receiving, counter, ejection timeout, sun sensors data processing, gyroscope data processing and ejection activation. The last three processes are implement as Moore finite state machines. The code for ejection algorithm is attached to Appendix A. Further discussion analyzes all processes independently. Figure 3-3 shows the structure of the ejection algorithm and an interaction of internal processes.



Figure 3-3 Ejection algorithm block diagram

3.2.1 Data receiving processes

Sun sensors data receiving and gyroscope data receiving processes have identical purposes. Both ejection ADC and gyroscope have their own controllers that output readings bytewise. The processes are responsible for data collection and packing into 64-bit signals for further processing. This is done by shifting in bytes of information when new data is ready.

3.2.2 Timing

In the ejection algorithm, two different systems of time are in use simultaneously, namely absolute and relative time. The absolute one starts counting when the FPGA is reset. It is represented with 21 bit vector, where the least significant bit (LSB) is changed every 0.5 ms. The other bits change their values with the frequencies shown in Table 3-1.

Bit position	Frequency
GLOBAL_TIME[0]	2 kHz
GLOBAL_TIME[1]	1 kHz
GLOBAL_TIME[2]	0.5 kHz
GLOBAL_TIME[11]	1 Hz
GLOBAL_TIME[20]	2 mHz

Table 3-1 Global time vector

Counter is a process that determines relative time between positions with the highest light intensity. In other words, it counts the time for one 360° rotation. It is triggered every half a millisecond and on a special signal from sun sensors data handling process, which occurs when a new maximum intensity is defined. After every new maximum value found the counter is reset.

3.2.3 Sun sensors data handling process

Direction of the ejection is tightly coupled with the Sun position. Sun sensors provide the FPGA with light intensity in real-time mode, what makes it difficult to determine a peak value on fly. This problem can be solved with introducing a margin, after which the attitude can be stated as a sun-directed. However, exact light intensity depends on many factors and is unknown, what, in turn injects additional sources of errors. For that reason, the following concept is implemented. Incoming new data is compared with a value stored in a variable, which is initialized with zero on the FPGA reset. If the new data is smaller than the data stored in the variable, the algorithm waits for next sun sensors data. Otherwise, the variable value is updated with the largest one. If the value of the variable has not been updated for last t ms, where t = T / 2 + 20 ms, then it corresponds to the maximum intensity value and in that moment the middle sun sensor was pointing onto the Sun. Adding the values from all three sources simplifies the implementation. In this case, a peak readout occurs when the source is straightly opposite the middle photodiode.

All three sun sensors readings are shown in Figure 3-4. Figure 3-5 represents the ADC data while the RMU was rotating on constant 3.05 Hz frequency on rotary table. The curves overlap without any glitch in between, what allows processing only a combined value instead of single readings. The resulting curve of the combined value is shown in Figure 3-6.

Figure 3-4 Sun sensors readings separately

Figure 3-5 Sun sensors readings

Figure 3-6 Sum of readings

Figure 3-7 Sun sensors data handling finite state machine

Every rocket rotation relative time of the determined maximum intensity is stored in a 1x4 array. These values are used for mean time calculation and more accurate time of the next peak intensity prediction.

A finite state machine for the above-discussed process, namely sun sensors data processing, is shown in Figure 3-7 and includes the following states:

S0: The state is triggered on every rising edge of the clock signal unless new data with a valid header is arrived. Upon arrival, all three single sun sensor readings are summed up and the process moves to the next state.

S1: If the new data has higher value than the one stored before, maximum value and its absolute time of occurrence is overwritten; otherwise, if no higher value has appeared during the time needed to pass 180° plus 20 ms since last stored maximum, the relative time of its appearance is stored in the array. The process starts from the beginning (S0) unless all four maximum values are found. After the fourth consecutive maximum intensity is defined, the process moves to the next state (S2).

S2: In this state first stage of mean time of 360° rotation is calculated. All four values from the time array are summed up.

S3: Result from S2 is divided by four. Division is implemented using bit shifting. Two bits are shifted to the right.

S4: The final state ensures mean time to be calculated and gives a flag to ejection activation process.

3.2.4 Gyroscope data handling process

All three sun sensors are located on the same side of the mechanical module as the lower FFU and according to the requirements, the FFUs shall be ejected perpendicularly to the Sun position. In order to fulfil the condition, time of 90° rotation is calculated using angular rate sensor readings. Figure 3-8 represents a finite state machine for gyroscope data processing.

Figure 3-8 Gyroscope data processing finite state machine

S0: When new valid data arrives, it is converted from two's complement to binary, preparations for division are done and the process goes to the next state. Otherwise, waits for new data.

S1: Division procedure is being done in this state. It is triggered 16 times. Time needed for 90° rotation is stored in a variable. Process continues with S0.

Output of the angular rate sensor is given in degrees per second (dps). Taking into account a sensitivity factor of 70 mdps/digit, desired value is a ratio of 1285714 and the gyroscope actual reading.

Division is implemented in sequential way by using a simple comparator and takes 16 clock cycles. The dividend is stored in a (n+k)-bit temporary buffer, where n is number of bits in a dividend and k is number of bits in a divisor. Every clock cycle buffer[(n+k-2) : (k-1)] is compared with the divisor. If the divisor is greater than the compared part of the buffer, the buffer is shifted one bit to the left. Otherwise, the buffer((n+k-1) equals to '0' and the buffer[(n+k-2) : k] equals to a difference of the buffer[(n+k-3) : (k-1)] and the divisor[(k-2) : 0]; '1' is shifted in to the right of the buffer[(k-1) : 0]. Current procedure is repeated k times. At clock cycle k the solution equals to buffer[(k-1) : 0] and the remainder equals to buffer[(n+k-2) : k].

The division example is shown in Table 3-2, where the dividend is 14 and the divisor is 5. The part of the buffer vector that is compared with the divisor is highlighted with red color. The divisor is a 4 bit vector in this example (k = 4), thus the whole procedure takes 4 clock cycles. At clock cycle number 4, the first 4 bits of the buffer correspond to the solution and the next three correspond to the remainder. The solution and the remainder for the given example is highlighted with blue and brown colors, respectively. Cycle 0 is used for preparation, namely shifting the dividend into the buffer vector and resetting counter.

CLK cycle	Buffer	Divisor
0	0000 1110	0101
1	0001 1100	0101
2	0011 1000	0101
3	0010 0001	0101
4	0100 0010	0101

Table 3-2 Division example

3.2.5 Ejection activation process

Ejection signal activation process starts execution only when sun sensors data handling process is in the final state (S4), which is called a flag state. After receiving a flag signal, ejection time is calculated taking into account mean time of one 360° rotation, mechanical and electrical delays as well as time of 90° rotation. Firing signal activates as soon as the calculated condition is met and the signal is kept high for 12 ms. A finite state machine for the ejection activation process is shown in Figure 3-9.

Figure 3-9 Ejection activation process finite state machine

The finite state machine has the following states:

S0: The entire process stores absolute time of the last maximum intensity and goes to the next state if sun sensors data handling process is in the final state (S3).

S1: Ejection time is calculated and state is changed to S2.

S2: If the absolute time is smaller than the calculated ejection time, then the ejection signal is low. Otherwise, it goes high, deactivation condition is calculated and state is changed to S3.

S3: The ejection signal is kept high until deactivation condition is met. When the absolute time reaches deactivation time, the ejection signal is forced to zero and state is changed to S0.

3.2.6 Ejection timeout process

Ejection is a very critical part of the experiment and it shall happen in any case even if some of the supporting parts as gyroscope, ADC or sun sensors malfunction. In order to ensure ejection of the FFUs, timeout procedure is implemented in the algorithm. The timeout signal activates every 4 s and stays high for 1 s. However, it is a backup signal and therefore, the activation condition is recalculated every time when the signal from the ejection activation process goes high, postponing timeout for another 4 s.

Undesirable ejection during testing procedures can lead to damages in the RMU module as well as in the FFUs. To avoid any accident, manual arming of the ejection is implemented as a safety measure. This is done by injecting an internal signal, which can be controlled only by an operator through a communication line. The resulting output signal of the whole algorithm is produced according to the following logic equation (2):

 $S = (S_{EJ} \lor S_{TO} \lor S_M) \land S_{ARM}$ (2), where

 S_{EJ} – signal from enable ejection process

- S_{TO} timeout ejection
- S_M manual activation signal
- SARM manual arm signal
- S resulting output of the ejection block
- V logic OR operator
- Λ logic AND operator

The manual activation signal is implemented for early stage verification purpose and measurement of electrical parameters of the circuit.

3.3 Communication

Some of the RMU functionalities require direct involvement of a ground station operator. During the final countdown preparations, camera mounted on the skin of the rocket shall be properly switched on and ejection system must be armed. Moreover, downlink provided by the RXSM makes it possible to monitor all the important parameters of the experiment both before and after liftoff.

The communication between ground station and the experiment is divided into two different sections: the RMU and the FFUs communication, respectively. Independently of a type, all messages are processed by the ISAAC RMU Controller, which is partially inherited from the MUSCAT experiment.

3.3.1 RMU communication

The RMU continuously sends housekeeping data packets to the ground station, which contain the most important data and allow monitoring the whole experiment's performance. Each 26 bytes real-time message has the structure shown in Table 3-3, where the HEADER is "#0" and it represents that the message contains the RMU related data.

Table 3-3 Real-time message structure

Real-time message					
HEADER	TIME	Binary zeroes	Status	HK data 1	HK data 2
16 bits	28 bits	24 bits	12 bits	64 bits	64 bits

Post-flight analysis requires careful data conversion and plotting all the readings versus time. This becomes possible due to TIME vector contained in the real-time message. The vector consists of three parts: 2-bit header, 18-bit vector for seconds since last FPGA reset and 8 bits for M_TIME [25:18] time vector. Changing frequencies of the last one are shown in Table 3-5 and the structure of the TIME vector is shown in Table 3-4.

Table 3-4 Time vector structure

Time vector					
Header	Seconds since reset	Time within seconds			
2 bits	18 bits	8 bits			

Tal	ble	3-5	"Time	within	ı a	second"	' vector
-----	-----	-----	-------	--------	-----	---------	----------

Bit number	Changing frequency			
M_TIME [18]	128 Hz			
M_TIME [19]	64 Hz			
M_TIME [23]	4 Hz			
M_TIME [25]	1 Hz			

Another important part of the real-time message is a status vector, which gives an overview of events happening in the FPGA. It consists of 12 bits, where every single bit is related to a specific event. The list of the events with corresponding bit number is shown in Table 3-6.
Bit	Event
STATUS_VECTOR[0]	Rotator
STATUS_VECTOR[1]	Maximum
STATUS_VECTOR[2]	Fire
STATUS_VECTOR[3]	Enable ejection
STATUS_VECTOR[4]	Camera button 1
STATUS_VECTOR[5]	Camera button 2
STATUS_VECTOR[6]	Camera power ON
STATUS_VECTOR[7]	Recording
STATUS_VECTOR[8]	RxCU sleep
STATUS_VECTOR[9]	RxSU sleep
STATUS_VECTOR[10]	TxCU sleep
STATUS_VECTOR[11]	TxSU sleep

Table 3-6 Status vector structure

The RMU sends real-time messages only in Rotator mode. The FPGA sends its data and asks for real-time data from every FFU by turn. The experiment is in rotator mode by default, however it can be deactivated by sending " ' " character. STATUS_VECTOR[1] changes its state when a new maximum intensity of the light is found. According to the ejection algorithm, it toggles in $t = t_{\frac{1}{2}} + 20$ [ms] after the maximum intensity is captured by photodiodes, where $t_{\frac{1}{2}}$ corresponds to the time needed to pass 180°. Fire event indicates the signal driven to the ejection system's power driver. In case of manual activation, character "P" shall be sent to the controller. Enable ejection shows the ejection arming status. By sending "E" character, the experiment can be armed or disarmed. Next 4 bits are related to camera control. The camera has two buttons and they are "pressed" automatically by an algorithm in this case. Moreover, all of these camera single events can be toggled by sending "*", "+", "," and "-", respectively. The ability of full control is very important taking into account that the camera is modified especially for the experiment. It has no battery and it is impossible to press buttons on the camera itself. In case of improper shutdown, the camera control algorithm will be terminated in a wrong state, what may lead to malfunctions. The last four bits indicate sleep/awake statuses of the FFUs and "#", "\$", "!" and " " " are the characters for switching state given in order as provided by the status vector.

The third important part of the real-time message is housekeeping data. The ground station operator receives all crucial readings provided by the ADCs and the angular rate sensor before and during the experiment execution in order to monitor correctness and readiness of the system.

Housekeeping data packets consist of information from several sources, which is sampled at different time slots. The housekeeping ADC digitalizes all FFUs' voltages and currents, what becomes uninteresting for the operator due to a down scope in the ISAAC experiment objectives. In order to receive only valuable information and simplify monitoring process, *data_sender* block was developed. Full VHDL code for the block is attached to Appendix B.



Figure 3-10 Data_sender: interaction of internal processes

Figure 3-10 illustrates the interaction of internal processes in the data_sender block. Full packages coming from the ADCs and the gyroscope are processed individually and necessary parts are stored in intermediate signals. The output vector generating process selectively combines intermediate signals into one 48-bit signal, which is being output adding a header in the beginning. The header for the packets has two different values: "01BE" and "02BE" for the first and the second housekeeping data packet, respectively.

Housekeeping data packet 1 contains sun sensors readings and its structure is shown in Table 3-7. The structure of the housekeeping data packet 2 is shown in Table 3-8. Data provided by both the ejection ADC and the gyroscope are combined in this packet.

	HK da	ata 1		
Header	Binary zeroes	SS1	SS2	SS3
16 bits	12 bits	12 bits	12 bits	12 bits

Table 3-7 Housekeeping data packet 1

Table 3-8	8 Housek	eeping	data	packet	2
-----------	----------	--------	------	--------	---

	НК	data 2		
Header	Temperature sensor	1.5V	Gyro temp	Gyro Z axis
16 bits	12 bits	12 bits	8 bits	16 bits

Table 3-9 illustrates an example real-time message received from the RMU.

Table 3-9 Real-time message example

#0	400362C	000000	F43	01BE00012516014D	02BEAEABB8120001
Header	Time		Status vector	Housekeeping data 1	Housekeeping data 2

3.3.2 General FFU communication

The ISAAC experiment has two different-purpose FFUs with identical CUs and different SUs. The TxSU is fully autonomous, however both CUs and the RxSU require communication lines for various operations with memories, status monitoring and flight preparations. FFU commands sent to the RMU are being processed by the ISAAC RMU Controller as it was in the previous case, however switching blocks are needed to redirect messages to the proper FFU. 3-to-1 multiplexer is implemented for a transmitting line and 1-to-3 demultiplexer for a receiving line. Channel selection is done by sending special characters to the controller, e.g. "1" for the TxCU, "2" for the RxCU, "3" for the RxSU and "0" for the RMU. After choosing a proper addressee, an internal communication line is redirected to its FPGA pins. The VHDL code for communication switches is attached to Appendix C.

3.3.3 RxSU communication

Although the RxSU has a complex structure with four different FPGAs, communication with it is done through a single line. A special switch implemented in the main FPGA, which is responsible for the FFU sun sensors data processing, ensures accessibility of every single FPGA. The main FPGA permanently listens to the communication line and redirects messages if one of the following ASCII characters appear: "%" for the sun sensors FPGA, "&" for the camera FPGA, "(" for the SmartFusion2 and ")" for the IR FPGA.

The implementation is separated into two blocks: a communication controller and a switch itself. The code for these blocks is brought in Appendix D. The switch is made in a multiplexer style, where the communication controller drives a selecting signal. The purpose of the switch is to internally connect proper FPGA pins with each other and pull-up unused ones.

3.3.4 GUI

Real-time communication with a ground station is done through serial port and it is nothing but a stream of packets, represented in hex format. Due to difficulties in following the readings using terminal, graphical user interface (GUI) Muscateer is used. The GUI is fully inherited from the MUSCAT experiment with some minor changes.



Figure 3-11 Ground station GUI

It is written in C++ programming language and adapted to the ISAAC experiment, because of distinctions in real-time message structure. Besides that, the ISAAC messages include some data, which are not compatible with the type declared in the initial version of the software. The angular rate sensor's data are represented in two's complement format and, thus, can have both positive and negative values. The adapted version has buttons for pre-flight preparations to minimize any accidental mistake occurrence, visualization for new statuses and proper conversion for raw data.

Any development is always followed by a verification phase. In this section, verification process of the RMU system is discussed. Depending on the part under test, verification is done using different methods. Some of them require simulations, other just a communication line or even a high definition camera.

4.1 Communication

The RMU PCB does not have any memory and this makes the communication line extremely important for the experiment. The main source of information for post-flight analysis is the messages received through downlink.

The verification procedure examines proper functionality of not only UART communication blocks implemented in the FPGA, but also the ADCs, the angular rate sensor as well as the ISAAC RMU Controller block. Only having all the above-mentioned blocks correctly functioning, the expected and the received data can match.

In order to obtain better resolution of diagrams, communication baud rate is increased to 115.2 Kbit/s for testing purpose. The ejection arm and the eject signals are illustrated in Figure 4-1. The diagram clearly shows proper functionality of both downlink and uplink. The eject signal appears only when the ejection algorithm is manually activated by the operator. The arm signal changes its value when the RMU receives "E" command from the ground station. Horizontal axis of the graph represents time after the FPGA reset.

Example log file is shown in Figure 4-2, where each line consists of one real-time message.



Figure 4-1 Uplink and downlink test

2	C:\Users\Rus\Desktop\launch_log.log - Notepad++ ×	
<u>F</u> ile <u>E</u> d <u>W</u> indow	lit <u>S</u> earch <u>V</u> iew Encoding <u>L</u> anguage Se <u>t</u> tings Macro Run Plugins / <u>?</u>	х
	} ⊟ 🖻 🗟 ∿ 😂 ∦ № 🖺 ⊅ ⊂ # 🌆 💁 🤹 🔍 🖾 🖾 🔜 1	»
📄 laund	ch_log.log	
1	#0403A3D4000000F0301BE00006E18725102BEAECBB80E0001	^
2	#0403A3F4000000F0301BE00007318824A02BEAFDBB80E0002	۰,
3	#0403A41C000000F0301BE00007918724C02BEAF5BB80E0000	
4	#0403A43C000000F0301BE00007218F25002BEAF1BB80E0006	
5	#0403A45C000000F0301BE00007118725502BEB08BB80E0004	
6	#0403A47C000000F0301BE00007618A24D02BEAE9BB70E0004	
7	#0403A49C000000F0301BE00006518A25602BEAF4BB70E0003	
8	#0403A4BC000000F0301BE00007018E24C02BEB02BB80E0004	
9	#0403A4DC000000F0301BE00006C18F25102BEAF3BB70E0006	
10	#0403A504000000F0301BE00007B18624D02BEAFDBB80E0005 ,	~
Ln:1 Co	ol:1 Sel:0 0 UNIX ANSI INS	

Figure 4-2 Log file

4.2 Camera

The GoPro Hero 3 camera is an independent device and its testing method lies in remote activation, record starting and automatic video saving after 660 s. Although it can be fully controlled through uplink, it is very difficult to perform remotely. In order to avoid any unexpected behavior, the camera was tested and critical cases, which can lead to malfunction, were discovered.

Figure 4-3 illustrates camera signals and their behavior according to the recording algorithm. Recording process lasts exactly 660 s, starting from t = 110 s and finishing at t = 770 s. However, the camera is not switched off, but recording is stopped, video is saved and a new one started. At t = 860 s the camera was turned off by the operator.

Incorrect shutdown inevitably leads to malfunction next time the camera will be used. Simple and effective remedy to have safe recording requires additional powering on the camera before any recording process. The principle is shown on the graph. The camera is switched on at t = 0 s and switched off at t = 80 s.



Figure 4-3 Camera signals

4.3 Ejection algorithm

Complex structure of the ejection algorithm requires several different approaches to verify completely the whole block. Verification process of all key blocks is discussed in this section. The angular rate sensor data is processed using mathematical division, which is verified separately.

Flight conditions for the RMU are simulated using a rotary table with adjustable rotational speed. To communicate with the rotating PCB is difficult having cables connected to the ground station. Solution was found in Wireless Bluetooth RF Transceiver Module serial RS232 TTL HC-05 [14].

4.3.1 Division

The implemented division block using VHDL hardware description language was verified using ModelSim simulation. Obtained waveforms are shown in Figure 4-4.



Figure 4-4 Division block simulation

All numbers are chosen as close as possible to the realistic ones. The dividend has the same value as in the ejection algorithm. Although the divisor will not be constant during the flight, the approximate rotation frequency is stated to be 3 Hz, which, in turn, is 1080 dps. Due to the fact that all terms of division belong to integer set, the fraction is omitted, what injects an additional error. In the examined example, the fraction value is 0.47(592), which equals to 0.514 ms or 0.56° of rotation.

4.3.2 Angular rate sensor readings

The gyroscope functionality is verified on the rotary table. A peculiarity of the installation is inability of drastic acceleration. Figure 4-5 shows the angular rate sensor's output during the test.



Figure 4-5 Gyroscope data

The rotary table was smoothly sped up to 1300 dps for a short time and then rotation speed was held at constant 3 Hz level for about 20 s. The output precisely follows the test bench's performance.

4.3.3 Sun sensors readings

The sun sensors output voltage is represented in Figure 4-6. The given graph is based on communication data received while the RMU was rotating at constant 3 Hz frequency. All three waveforms overlap, which allows to process a combination of them instead of single readings, as it was mentioned before.



Figure 4-6 Sun sensor data

Analyzing the graph, approximate period can be calculated.

70.1 - 69.75 = 0.35 s, where 70.1 s and 69.75 s are the time values for two consecutive peaks of the blue waveform.

The difference is 0.35 s, which is close to 333 ms for 3 Hz frequency.

The results fully correspond to the expectations.

4.3.4 Sun sensors data handling

The purpose of the sun sensors data handling process is to follow the ejection ADC data and search for maximum light intensity. The combined sun sensors readings and the maximum signal are illustrated in Figure 4-7. Every half of a rotation period plus 20 ms the maximum signal changes its value to the opposite. Time, when the signal is constant high or constant low, equals to relative time of one 360° rotation.



Figure 4-7 Maximum light intensity identification

Analyzing the graph, it is clearly seen that the maximum signal edges are slightly to the right from lines of symmetry between two consecutive peaks. Besides that, every peak intensity point is properly identified by the algorithm, what makes this process fully meeting the requirements.

4.3.5 Arming procedure

The ejection algorithm executes continuously, however the output is blocked by the arm signal. This preventing mechanism is shown in Figure 4-8. The diagram illustrates behavior of the output under different arm signal states. Disabling the arm signal is an important safety measure, which allows to prevent unanticipated ejection.





The signal is controlled by the ground station operator and it shall be activated before liftoff due to absence of uplink during flight.

4.3.6 Ejection timeout

The timeout process is implemented as an alternate ejection method in case of malfunctions in the gyroscope, the photodiodes or the ADC. The operation principle of the process is shown in Figure 4-9.



Figure 4-9 Timeout signal

The timeout process forces the output to logic 1 for 1 s. In accordance with the graph, it is high from 15.4 s to 16.4 s and 22.5 s to 23.5 s. The activation condition is 4 s without any activity in the output signal. Absence of the signal at t = 20.4 s proves its secondary importance, namely, every eject signal appearance postpones the timeout condition for another 4 s.

4.3.7 Ejection activation process

Another important part to verify is correctness of the eject signal activation time. The process calculates the time of every fifth consecutive peak intensity appearance and ejects the FFUs, taking into account delays. Figure 4-10 proves the before-mentioned algorithm.

At approximately t = 330.2 s the first maximum intensity in captured. The second peak appears at t = 330.5 s. The third one is at 330.8 s and the last is at 331.2 s. After all 4 values are found, the ejection signal goes high at 331.4 s, just before the next peak intensity because of mechanical delay.



Figure 4-10 Ejection activation algorithm

4.4 Environmental tests

Under conditions of absence of convectional cooling and temperature differential during countdown, launch and flight, experiment electronics must be tested to ensure nominal operation in all the worst cases. For that reason, vacuum and thermal test are conducted.

4.4.1 Vacuum test

Vacuum test was conducted using a special vacuum chamber provided by the university. The range of pressure inside the chamber varies from normal room pressure in the lab down to 80 microns Hg (0,1067 mbar). The flight mode of the RMU PCB was activated during the test.



Figure 4-11 Vacuum chamber

In order to reach such low pressure inside the vacuum chamber and keep ability to power on the PCB, special adapter was made. The cable, shown in Figure 4-12, has two D-SUB 15 connectors with a sealing adapter in between, which prevents airflow from outside the chamber.



Figure 4-12 RMU power cable for vacuum test

The RMU housekeeping data was logged for 700 ms when vacuum conditions were established. Decoded data is represented below in Figure 4-13.

The diagram illustrates stability of the RxSU and the TxSU supply voltage. Several different circuits take part in output voltage generation. The RMU is powered with 28V, which is

further converted into 4.2V, 3.85V for the FFUs and 5V. The last, in turn, is converted into 3.3V for feeding digital electronics. A stable final stage ensures stability in all previous stages. Moreover, continuity of the time axis confirms uninterrupted operation of the FPGA.



Figure 4-13 Output voltage under vacuum condition

4.4.2 Thermal test

The RMU electronics behavior under temperature variation was tested in a special thermal chamber. The entire test was conducted in two phases: a hot test and a cold test. Peak temperatures for these tests were +60°C and -30°C, respectively. The RMU data was being recorded during the temperature variation process as well 15 minutes after temperature was stabilized.

Voltage behavior across the temperature variation is nominal with maximum deviation of 1.5% and 2.3% for the hot and the cold test, respectively. The calculations are based on the data represented in Figure 4-14 and Figure 4-15.

Heating:

3.894 - 3.836 = 0.058 V

 $0.058 \div 3.836 \cdot 100\% = 1.5\%$

Cooling:

3.832 - 3.744 = 0.088 V $0.088 \div 3.744 \cdot 100\% = 2.3\%$

Both the FFU's supply voltage and the temperature inside the chamber follow the same trend. Maximum deviation of the voltage trace is 0.058V (Figure 4-14) under heat effect and 0.088V (Figure 4-15) under cold effect.



Figure 4-14 Heat influence on voltage

The reason for changes in output voltage is resistance and temperature relationship, which is described with the following equation (3):

 $R = R_{ref} \cdot [1 + \alpha (T - T_{ref})] \quad (3), \text{ where }$

R - Conductor resistance at temperature T,

 R_{ref} – Conductor resistance at reference temperature T_{ref}

 α – Temperature coefficient of resistance for the conductor material

T – Conductor temperature in degrees Celsius

 T_{ref} – Reference temperature that α is specified at for the given conductor material

The above-mentioned equation proves the behavior of the voltage traces. Any change in temperature cause a change in aggregate resistance of the electrical circuit.

Unexpected short-time temperature fall in Figure 4-14 at time t = 1700s can be caused by improper actions of a test operator.

The diagram related to the influence of cold clearly recognizes a problem. At temperature levels of -18°C and -30°C, the FPGA resets. The malfunction appeared when the 18-bit time vector value reached 1023, however this problem does not occur during the hot test. Recommended operation conditions for ProAsic3 Family FPGAs lie between -40°C and +85°C [6] and the test conditions are close to the boundary ones. Further investigation of this phenomenon needs to be done.



Figure 4-15 Cold influence on voltage

The launch campaign was held in Esrange, Kiruna from 19th of May until 1st of June 2014 with the launch itself on 29th of May. All real-time data before, during and after liftoff were properly logged, what allows to analyze the RMU functionality during the flight.

The experiments on-board the rocket were activated 600 s before liftoff and switched off 600 s later. Unfortunately, the FPGA reset at time t = 1024 s. However, all the most crucial data for the ISAAC experiment is collected and the malfunction had no serious impact. In general, all parts developed during the degree project time successfully accomplished the task and the further analysis proves that.

Peak spinning rate reached during the whole flight is 1408.12 dps at time t = 621.516 s. Angular velocity is plotted in Figure 5-1. Real-time communication packets of the ISAAC experiment do not allow to define exact ejection moment. The problem is solved using data provided by the FOVS experiment. Figure 5-2 illustrates accelerometer's reading in time interval from 90 s to 100 s after liftoff. According to the diagram, the ejection of the FFUs was approximately at time t = 691 s after the experiment activation. At the moment of ejection, rotation speed of the rocket was 1092.4 dps, which is very close to the expected one.

Behavior of the photodiodes is shown in Figure 5-3. Analyzing the traces, the graph can be divided into 3 stages with t_1 as a starting point and t_2 as a finishing point of the time interval.

 $t_1 = 590$ s, $t_2 = 600$ s: The rocket is in stationary state on the ground and the photodiodes do not point in the Sun direction.

 $t_1 = 600$ s, $t_2 = 700$ s: The rocket is in flight. Active phase of the experiment.

 $t_1 = 700$ s, $t_2 = 800$ s: Yo-yo de-spin with further stable and very slow rotation speed.



Figure 5-1 Angular velocity of the rocket



Figure 5-2 Accelerometer data



Figure 5-3 Sun sensors and gyro behavior during the flight

Maximum output voltage of the sun sensors is 1.4 V which proves the correctness of the chosen amplification gain.

Video recording related signals are shown in Figure 5-4. Due to malfunction in the FPGA and its unexpected reset, the flight video stops just after the Yo-yo de-spin.



Figure 5-4 Camera signals

Some housekeeping data is illustrated in Figure 5-5. The temperature sensor is mounted on the aluminum rocket skin, which is heating very fast due to friction. FPGA supply voltage is constant during the whole period. Neither temperature change nor vacuum had any impact on the electrical parameter.



Figure 5-5 Housekeeping data

Duty cycle of the eject signal is very low, because it goes high only for 12 ms. Figure 5-6 illustrates a time window of the ejection. Readings of accelerometer show that ejection was in the interval from 690s to 692s, however, the signal is absent. The reason for that is low communication speed and messages with high eject signal are lost. Figure 5-7 is a good evidence for that. The diagram shows the closest eject signal triggered before. If there were no any short ejection signal after, the timeout process would definitely force the eject signal high for 1s.



Figure 5-6 Sun sensors readings during the ejection moment



Figure 5-7 Example of ejection signal

Presence of the camera allows making a video analysis of the ejection. Figure 5-8 and Figure 5-9 illustrate video frames 27224 and 27243, respectively. The camera was set to 240 frames per second recording, what makes it possible to examine a picture every 4.17 ms. A thin black line at the bottom right hand corner of Figure 5-8 is a hatch. It is the first appearance of any part involved in the ejection procedure and, thus, the frame is stated as the beginning of the ejection process. On the other hand, Figure 5-9 has the Sun in the middle and this frame shall be 90° far away from the starting point of the ejection. Taking into account the angular rate sensor reading, the angular velocity during the ejection was 1092.4 dps or rotational frequency was 3.034 Hz. Having all this information the actual and the proper moment of ejection is calculated below.

$1 \div 240 = 0.0041(6) \ s \approx 4.17 \ ms$	time between 2 consecutive frames
27243 – 27224 = 19 frames	number of frames
$4.17 \cdot 19 = 79.23 ms$	time between frames
$1092.4 \div 360 = 3.03(4) Hz$	rotation frequency
$1 \div 3.03(4) \approx 0.329 s = 329 ms$	time to pass 360°
$329 \div 360 \cdot 90 = 82.25 ms$	time to pass 90°



Figure 5-8 Ejection video frame 27224



Figure 5-9 Ejection video frame 27243

In order to pass 90° with a constant speed of 1092.4 dps, 82.25 ms are needed. The time calculated using video analysis is 79.23 ms without consideration of uncertainty, which is caused by the minimal time unit of 4.17 ms, imprecise selection of a starting frame and angular rate sensor's accuracy. Possible solutions to improve ejection timing are discussed in the discussion section.

$90 - 79.23 \cdot 90 \div 82.25 = 3.3^{\circ}$	deviation angle
82.25 - 79.23 = 3.02 ms	deviation time

According to the calculations, the ejection took place 3.3° or $3.02*10^{-3}$ s earlier than it should have happened. The obtained deviation is smaller than the time between two consecutive frames. The result fully corresponds to the requirement.

The degree project is focused on the RMU electronics development and validation, what is clearly documented in previous chapters. The designed and implemented firmware for the RMU FPGA resulted in successful ejection control with informative real-time communication packets and high-definition video. Several new features for the ISAAC experiment were developed as well as adapted and improved the inherited ones.

A foundation of the ejection algorithm is the ability of the module to correctly identify the Sun position. Three stand-alone sun sensors were developed with the appropriate amplification gain, which matches the output with the reference voltage of the ADC. The proper gain of 3.5 was found empirically and the correctness is proved in the post-flight analysis.

The complex ejection algorithm was developed and implemented in VHDL hardware description language with interaction of seven concurrent processes. The verification phase of every single process as well as the post-flight analysis demonstrate its full compliance with the requirements. However, there is a way to improve the accuracy of the ejection, which is left for a future work. Mechanical delay of the FFUs ejection is found empirically during dynamic ejection tests and it is declared as a constant variable. In order to improve ejection timing, more test should be conducted with the FFUs of the same mass as the ones for a flight. Different delay values can be injected into the algorithm switching a value depending on the actual angular velocity.

Another important part of the developed firmware is the communication. The implemented block provides a ground station operator with all crucial and interesting information during flight; however, it has a serious drawback. The communication speed of downlink is slow and a lot of information is lost. Moreover, the block itself slows down twice a real-time message sampling rate, because it consists of two different vectors and each of them is sampled on the rising edge of the write enable signal. Despite an artificial decrease of the communication speed, it is fast enough for real-time monitoring in the GUI. For future work some improving suggestions can be given, namely to use flash memory as a storage for the real-time data and to change structure of the output_vector process in the data_sender block. Changing value of the mixed_data signal using a time vector as a triggering event will allow to get rid of necessity to wait until rising edge

of the write enable signal and therefore to increase the communication speed. Supplementing flash memory will make a post-flight analysis independent on downlink speed.

The video recording algorithm for a GoPro Hero 3 camera was improved adding a possibility to switch on and off the camera without recording. The present option is important to avoid malfunctions after an improper camera shutdown.

The entire conducted work showed itself as successful and meeting all the requirements.

For future work, necessity of accelerometer and another camera should be investigated. Having accelerometer on the PCB, the ejection moment can be analyzed more precisely. The camera in the ISAAC experiment is mounted above the bottom FFU and starting ejection moment is clearly identifiable. However, due to mechanical construction, the bottom FFU is ejected later than the top one. Another camera below the top FFU will allow to make better analysis of the ejection.

Moreover, unsuitable behavior of the FPGA at time t = 1024 s needs further investigation.

The RMU electronics for the ISAAC experiment was developed and implemented in this Master's Thesis. The RMU PCB and sun sensors PCBs were soldered, troubleshot and verified. The FPGA firmware, which embraces newly implemented ejection algorithm, real-time communication processing blocks and many others inherited from the previous experiments, was implemented in VHDL hardware description language with following validation.

The ISAAC experiment was launched on-board the REXUS15 sounding rocket on May 29 from Esrange, Kiruna. All real-time data messages were properly logged and used in the post-flight analysis for validation of the ejection algorithm. The data received during the active phase of the experiment is complete and reasonable. Unfortunately, a malfunction occurred in the FPGA in 1024 s after powering on the experiment. However, it affected only the video, having stopped it after 236 s of recording.

The results obtained in the verification phase and the post-flight analysis prove a success in reaching the objectives of this thesis work.

Lõputöö on keskendutud Rocket Mounted Unit (RMU) elektroonika arendamisele ning valideerimisele, mis on selgelt dokumenteeritud eelmistes peatükkides. Disainitud ja rakendatud RMU programmeeritava ventiilmaatriksi (ingl.k. Field-Programmable Gate Array, FPGA) tarkvara tulemuseks oli edukas väljaheitmise kontroll ning reaalajas saadud informatsioon vastas püstitatud nõuetele. ISAAC eksperimendi jaoks olid väljatöötatud mõned uued ja jäetud mõned vanad eelmistest projektidest päritud, kuid adapteeritud ja parendatud funktsioonid.

Väljaheitmise algoritmi eesmärgiks on päikese asukoha korrektne tuvastamine ehk maksimaalse hälvega ±20°. Arendati kolm iseseisvat päikeseandurit kindla võimendusteguriga, mis ühtib analoog-digitaalmuunduri (ADC) väljundi nominaalse pingega.

Sobiv 3.5 võimendustegur oli leitud empiiriliselt, meetodi korrektsus sai tõestatud läbiviidud lennujärgse analüüsiga.

Väljaheitmise algoritm oli välja töötatud ning rakendatud kasutades VHDL riistvara kirjeldamise keelt. Käesoleva algoritmi keerulisus oli tingitud sellest, et samaaegselt pidi toimima seitse üksteisest sõltuvat protsessi. Arendatud algoritmil on järgmine põhimõte. Valguse intensiivsus ja nurkkiirus mõõdetakse pidevalt päikeseandurite ja nurkkiiruseanduri abil. Juhul kui mõõdetud näide on suurem kui varem salvestatud, vana muutuja väärtus ülekirjutatakse. Väiksema näide korral lõplik olekumasin (ingl.k. finite state machine) jätkab algusest peale ehk ootab järgmist näidet. Kui nurkkiirus on teada, teine protsess arvutab 90° pööramise aja. Kui viimase t ms jooksul, kus t = T/2 + 20 ms, valguse intensiivsuse muutuja pole kordagi ülekirjutatud, muutuja viimase ülekirjutamise aeg vastab asendile, millal keskmine päikeseanduri ja päike vahel on nurk 0°. Väljaheitmise täpsuse tõstmise jaoks arvutatakse matemaatilist keskmist väärtust neljast pöördest ja prognoseeritakse järgmise maksimumi aeg. Kuna FFU moodulid peavad olema väljalastud päike suhtes risti, prognoseeritud ajale lisatakse aeg vajalik 90° pöörlemiseks ning lahutatakse mehhaanilisi ja elektrilisi viivitusi. Iga iseseisva protsessi kontrollimise etapp ning läbiviidud lennujärgne analüüs demonstreerisid täielikku vastavust püstitatud nõuetele. Siiski on olemas viis väljalaskmise täpsuse parandamiseks, millega planeeritakse jätkata tulevikus. Vabalangeva seadme (ingl. k. Free-Falling Unit, FFU) mehhaaniline väljaheitmise hilinemine oli leitud empiiriliselt dünaamilise väljaheitmise testi jooksul ning selle testi tulemus oli juurutatud algoritmi konstantse arvuna. Väljaheitmise ajastuse parendamiseks tuleb läbi viia rohkem katseid kasutades samasuguse massiga FFU'd nagu need, mida kasutatakse tulevasel lennul. Erinevaid viivituse väärtusi võib juurutada algoritmi ning vahetada väärtust vastavalt tegelikule nurkkiirusele.

Teine oluline arendatud osa selles lõputöös on kommunikatsioon operaatori ja mooduli vahel. Käesoleva lõputöö üheks olulisemaks osaks on lennujärgne analüüs, mis nõuab erinevate andmete kogumist. Rakendatud plokk annab maapealsele operaatorile kõige olulisemat ja huvitavat informatsiooni reaalajas lennu ajal. Eksperimendi tipp kõrguseks oli ligikaudu 90 km. Sellel kõrgusel puudub konvektsioon, mis omakorda võib kutsuda esile elektroonika ülekuumenemist ja parameetrite muutumist. RMU nominaalne toitepinge on 28 V, mis edaspidi muundatakse 5 V-ks, 4.3 V-ks, 3.3 V-ks ja 1.5 V-ks. Muundumise viimaseks astmeks on 1.5 V FPGA toitmiseks, mis oli valitud üldise elektroonika seisu kontrolli jaoks. Kui muunduri väljund vastab 1.5 V-le, siis võime järeldada, et RMU elektroonika on töökorras. Väljaheitmise algoritmi analüüsimiseks saadetakse maapealsele operaatorile kõik need andmed, mis sadeti algoritmile parameetritena välisandurite poolt ehk päikeseandurite ja nurkkiiruseanduri poolt. Samuti oli salvestatud mooduli kere peale paigaldatud temperatuurianduri näidud.

Rakendatud kommunikatsiooni plokk võimaldas nii andmete kui ka eksperimendi käigu staatuste kättesaamist reaalajas. Siiski leidub sel tõsine puudus. Kommunikatsiooni downlink kiirus on madal, mille tõttu mõned informatsiooni paketid lähevad kaotsi. Lisaks sellele aeglustab plokk ise väljundsignaali genereerimist kaks korda. Üks sõna koosneb kahest erinevast vektorist ja nad omakorda väljastatakse write enable signaali tõusval serval. Vaatamata kunstliku side kiiruse langusele on see piisavalt kiire, et reaalajas jälgida graafilist kasutajaliidest (ingl.k. Graphical User Interface, GUI). Tulevikus sarnaste projektide parendamiseks oleks mõistlikum kasutada flash mälu andmete salvestamiseks, mis kaotaks andmete üleandmise kiiruse mõju. Output_vector protsessi struktuuri muutmine data_sender plokis võimaldaks suurendada üleandmise kiirust kuni kaks korda. Täiendades elektrilist skeemi flash mäluga, muutub lennujärgne analüüs sõltumatuks downlink kiirusest.

Videosalvestuse algoritm GoPro Hero 3 kaamera jaoks oli parendatud lisades kaamerale võimaluse lülitada sisse ja välja ilma videosalvestamise käivitamiseta. Käesolev võimalus on oluline, et vältida tõrkeid pärast ebakorrektse kaamera väljalülitamist.

Kogu teostatud töö osutus edukaks ja vastab kõigile püstitatud nõuetele.

Tulevikus sarnastes projektides tuleb uurida võimalust paigaldada kiirendusmõõtur (ingl.k. angular rate sensor) ja lisa GoPro kaamera. Väljalaskmise momendi täpsemaks tuvastamiseks on otstarbekam lisada kiirendusmõõtur elektrilisele skeemile. ISAAC moodulis on kaamera paigaldatud alumise FFU peal ja seetõttu väljalaskmise momenti on selgelt näha. Lisades teise kaamera ülemise FFU alla, annab lennujärgne analüüs võimaluse määrata mehhaanilist viivitust. Mehaanilise konstruktsiooni omapära tõttu põhja FFU väljalaskmine toimub varem kui ülemise FFU.

Lisaks FPGA sobimatu käitumine ajahetkel t = 1024 s vajab edasist uurimist.

ISAAC eksperimendi RMU elektroonika oli väljatöötatud ning rakendatud käesolevas magistri lõputöös. RMU PCB ja päikese andurite PCBs olid joodetud, seadistatud ja kontrollitud. FPGA tarkvara, mis hõlmab hiljuti elluviidud väljaheitmise algoritmi, reaalajas kommunikatsiooni töötlemise plokke ja palju teisi sarnastest projektidest päritud kogemusi, oli rakendatud kasutades VHDL riistvara kirjeldamise keelt ning järgnevalt valideeritud.

ISAAC mooduli lennutati 29. mail Esrange polügoonilt REXUS15 raketi pardal.

Peatükis 5 on kirjeldatud lennujärgne analüüs koos tulemustega. Väljalaskmine pidi juhtuma ristloodi päike suhtes maksimaalse hälvega $\pm 20^{\circ}$. Algoritm tõestas oma töökindlust kuna eksperimendi ajal väljalaskmine toimis 3.3° või 0.0032s varem.

Kõik saadud reaalajas andmed olid salvestatud ilma vigadeta ning kasutatud lennujärgnevas analüüsis. Lennu ajal saadud informatsioon on lõplik ja korrektne. Kahjuks rike tekkis 1024 s peale mooduli sisselülitamist, kuid see mõjutas ainult videod katkestades salvestamist.

Reaalajas saadud näidud ja lennujärgne analüüs järeldavad, et käesoleva lõputöö eesmärgid on saavutatud.

BIBLIOGRAPHY

- [1] REXUS/BEXUS homepage http://www.rexusbexus.net/. Last visited 24.08.2014.a.
- [2] MUSCAT (RX13) SED v5.1, September 24, 2013
- [3] RAIN (RX11) SED v3.0, September 7, 2011
- [4] ISAAC (RX15) SED v4.2, March 17, 2014
- [5] A. Håkansson, Portal of Research Methods and Methodologies for Research Projects and Degree Projects. WORLDCOMP'13 - The 2013 World Congress in Computer Science, Computer Engineering, and Applied Computing, 22-25 July, 2013 Las Vegas, Nevada; USA.
- [6] Microsemi ProASIC3 Flash Family FPGAs datasheet.
- [7] L3G4200D Gyroscope datasheet.
- [8] SLSD-71N6 Solderable planar photodiode datasheet.
- [9] MAX 11617 12-bit ADC datasheet.
- [10] N-channel SIPMOS BSP318S datasheet.
- [11] TRW Airbag Systems GmbH Cutter 77003198 Typ A datasheet
- [12] B. Razavi, Design of Analog CMOS Integrated Circuits, New York: McGraw-Hill, 2001, 684 pages, ISBN-10: 0072380322.
- [13] LM7321 Operational amplifier datasheet.
- [14] Wireless Bluetooth RF Transceiver Module serial RS232 TTL HC-05 datasheet.

Appendix A:

Ejection algorithm

-- Ejection.vhd library IEEE;

use IEEE.STD_LOGIC_1164.all;

use IEEE.STD_LOGIC_UNSIGNED.ALL;

use ieee.std_logic_arith.all;

entity EjectionControl is	
PORT (
CLK	: in std_logic;
RESET	: in std_logic;
Ejection_ENABLE	: in std_logic;
M_TIME_0	: in std_logic;
M_TIME_14	: in std_logic;
From Ejection ADC	
New_Sun_Data	: in std_logic;
SunSensors	: in std_logic_vector(7 downto 0);
From Gyro	
New_Gyro_Data	: in std_logic;
GyroData	: in std_logic_vector(7 downto 0);
Ejection	-
manual_activation	: in std_logic;
ejection_test	: out std_logic;
ejection_1	: out std_logic
);	-
end EjectionControl;	

ARCHITECTURE behaviour OF EjectionControl IS

signal GLOBAL_TIME	: std_logic_vector (20 downto 0);
signal timeout_5s	: std_logic := '0';
signal SS_packed	: std_logic_vector (63 downto 0);
signal Gyro_packed	: std_logic_vector (63 downto 0);
signal ss_max	: std_logic_vector (12 downto 0);
signal ss_max_time	: std_logic_vector (20 downto 0);
signal reset_cond	: std_logic_vector (20 downto 0);
signal ss_LASTmax_time	: std_logic_vector (20 downto 0);
signal SS_sum	: std_logic_vector (12 downto 0);
signal time_90_deg	: std_logic_vector (15 downto 0);
signal timeout_time_5	: std_logic_vector (9 downto 0);
signal pyro_activation_int	: std_logic;

signal state	: std_logic_vector (3 downto 0);
signal buffer_div	: std_logic_vector(31 DOWNTO 0);
signal cnt_div	: std_logic_vector(4 DOWNTO 0);
signal gy_data	: std_logic_vector (15 downto 0);
signal time_array_avg	: std_logic_vector (11 downto 0);
signal time_array_avg2	: std_logic_vector (9 downto 0);
signal count	: integer range 0 to 3;
signal flag	: std_logic;
type matrix is array (3 downto 0) of	std_logic_vector (9 downto 0);
signal flag_old : std_logic;	
signal time_array	: matrix;
signal timeout_cond	: std_logic_Vector (9 downto 0);
· · · · 1 · · · · · · · · ·	
signal state4	: std_logic_vector (2 downto 0);
constant delay	: std_logic_vector (11 downto 0) := $x'' 120''$; 144.125 ms {144ms FFUout
delay + 4.125ms activation delay}	
constant zero_vector	: std_logic_vector (23 downto 0) := (others =>'0');
constant zero_vector2	: std_logic_vector (34 downto 0) := (others =>'0');
constant deg_per_ms	: std_logic_vector (23 downto 0) := $x''139E52''$; 90 * 1000 * 1000 / 70
signal condition1	: std_logic_vector (20 downto 0);
signal condition2	: std_logic_vector (20 downto 0);
signal state2	: std_logic_vector (3 downto 0);
signal counter	: std_logic_vector (9 downto 0);
signal ejection_test_int	: std_logic;

begin

ejection_1 <= (timeout_5s OR pyro_activation_int OR manual_activation) AND Ejection_ENABLE;

ejection_test <= ejection_test_int;</pre>

```
timer:process (M_TIME_14,RESET)
begin
  if RESET ='1' then
    GLOBAL_TIME <= (others => '0');
  elsif rising_edge (M_TIME_14) then
    GLOBAL_TIME <= GLOBAL_TIME + 1;
  end if;
end process;</pre>
```

```
SS_data_packer:process(M_TIME_0, RESET)
begin
if RESET='1' then
SS_packed <= (others => '0');
elsif rising_edge(M_TIME_0) AND New_Sun_Data='1' then
if New_Sun_Data='1' then
SS_packed <= SS_packed(55 downto 0) & SunSensors;
end if;
end if;</pre>
```
end process;

SS_combine : process (RESET, CLK)

```
begin
     if RESET = '1' then
       SS sum
                           \langle = (others = 0');
                           <= (others => '0');
       ss_max_time
                           \langle = (others = \rangle '0');
       ss_max
       time_array_avg
                           <= (others => '0');
       time_array_avg2 <= (others => '0');
                           <= (others =>(others =>'0'));
       time_array
                           \langle = (others = \rangle '0');
       reset_cond
                           <= '0':
       flag
       count
                           <= 0;
                           <= x"0";
       state2
       ejection_test_int <= '0';
    elsif rising_edge (CLK) then
       case state2 is
          when x''0'' =>
                  if New_Sun_Data = '0' AND SS_packed (63 downto 48) = x"01AD" then
                     SS_sum <= ('0' & SS_packed(11 downto 0)) + ('0' & SS_packed(23 downto 12)) + ('0' &
SS_packed(35 downto 24));
                     state2 <= x''1'';
                 else
                     state2 <= x"0";
                  end if;
          when x"1" =>
                  time_array(count) <= counter;</pre>
                  if ss_max < SS_sum then
                    ss_max <= SS_sum;
                    ss_max_time <= GLOBAL_TIME;
                    reset_cond <= GLOBAL_TIME + (time_90_deg & "00" + x"28");
                    state2 <= x''0'';
                  else
                    state2 <= x"0";
                    if GLOBAL_TIME(20 downto 0) > reset_cond then
                         flag <= not(flag);
                         ejection_test_int <= not (ejection_test_int);</pre>
                         ss_max <= (others \Rightarrow 0');
                         case count is
                                    when 3 =>
                                              state2 <= x"2";
                                              \operatorname{count} \langle = 0;
                                    when others \Rightarrow count \leq count + 1; state 2 \leq x''0'';
                         end case;
                     end if;
```

end if;

```
when x"2" =>
                       time_array_avg \le ("00" \& time_array(0)) + ("00" \& time_array(1)) + ("00" \& time_array(2))
+ ("00" & time_array(3));
                       state2 <= x"3";
          when x"3" =>
                       time_array_avg2 <= time_array_avg (11 downto 2);
                       state2 <= x"4";
          when x''4'' =>
                       state2 <= x"0";
          when others =>
                       state2 <= x"0";
          end case;
     end if:
  end process;
max_counter : process (M_TIME_14, RESET, flag)
begin
  if RESET = '1' then
     counter \leq (others \geq '0');
     flag_old \leq 0';
  elsif rising_edge (M_TIME_14) then
     if (flag_old = flag) then
       counter \leq counter + 1;
     else
       counter \leq (others \geq '0');
     end if;
     flag_old <= flag;
  end if;
end process;
enable_ejection : process (CLK,RESET)
  begin
    if RESET = '1' then
     state4 <= "000";
     pyro_activation_int <= '0';</pre>
     condition 1 \le (\text{others} => '0');
     condition 2 \le (\text{others} \implies 0');
     ss_LASTmax_time <=(others => '0');
 elsif rising_edge(CLK) then
     case state4 is
       when "000" =>
         if (state2 = x"4") then
             ss_LASTmax_time <= ss_max_time;</pre>
            state4 <= "001";
         else
             state4 <= "000";
         end if;
       when "001" =>
             state4 <= "010";
```

```
condition1 <= ss_LASTmax_time + (time_array_avg2 & '0') +(time_90_deg & '0') - delay;
       when "010" =>
           if GLOBAL_TIME < condition1 then
                 pyro_activation_int <= '0';</pre>
                 state4<= "010";
           else
                 condition2 \le condition1 + x"18"; -- +12 ms
                 state4 <= "011";
            end if:
       when "011" =>
          if GLOBAL_TIME < condition2 then
                 pyro_activation_int <= '1';</pre>
                 state4 <= "011";
           else
                 pyro_activation_int <= '0';</pre>
                 state4 <= "000";
           end if:
       when others => state4 <= "000";
    end case;
 end if:
end process;
Gyro_packer:process(M_TIME_0, RESET)
  begin
    if RESET='1' then
       Gyro_packed <= (others => '0');
      elsif rising_edge(M_TIME_0) and New_Gyro_Data='1' then
       if New_Gyro_Data='1' then
         Gyro_packed <= Gyro_packed(55 downto 0) & GyroData;
       end if:
    end if;
  end process;
Gyro_data_packer:process(CLK, RESET)
  begin
    if RESET='1' then
      time_90_deg <= (others = '0');
       gy_data \ll (others \implies '0');
       state <= x"0";
       cnt_div <= (others => '0');
       buffer_div \leq (others \Rightarrow '0');
    elsif rising_edge(CLK) then
       case state is
        when x''0'' =>
                 if (New_Gyro_Data='0' AND Gyro_packed (63 downto 56) = x"0C") then
                 ----- 2's complement to binary ------
                   if Gyro_packed (15) = '1' then
                     gy_data <= not(Gyro_packed (15 downto 0)) + x"1";
                   else
                      gy_data <= Gyro_packed (15 downto 0);
```

```
end if:
                  -----
                    state \leq x''1'';
                    cnt_div <= "00000";
                    buffer_div <= x"00" & deg_per_ms;</pre>
                  else
                    state <= x"0";
                  end if;
         when x''1'' \Rightarrow
                                    -- division state
                  if buffer_div(30 DOWNTO 15) \geq gy_data then
                    buffer_div(31 \text{ downto } 16) \le 0' \& (buffer_div(29 \text{ downto } 15) - gy_data(14 \text{ downto } 0));
                    buffer_div(15 downto 0) <= buffer_div(14 downto 0) & '1';</pre>
                  else
                    buffer_div \leq buffer_div((30) downto 0) & '0';
                  end if;
                  if cnt div = "10000" then -- 16 cycles
                    cnt_div \le cnt_div + 1;
                    state <= x"1";
                  else
                           -- Division is done
                    time 90 deg \leq buffer div(15 downto 0);
                    state <= x"0";
                  end if:
                  when others =>
                    state \leq x''0'';
                  end case;
     end if;
  end process;
timeout_ejection: process (CLK,RESET,pyro_activation_int)
begin
     if RESET = '1' then
       timeout_5s <= '0';
       timeout_time_5 <= (others => '0');
       timeout_cond <= "00" & x"04";
     elsif rising_edge (CLK) then
       timeout_time_5 <= GLOBAL_TIME(20 downto 11);</pre>
       if pyro_activation_int = '1' then
         timeout_cond <= GLOBAL_TIME(20 downto 11) + x"4";
       end if;
       if (timeout_time_5 < timeout_cond) then
            timeout_5s <= '0';
       elsif (timeout_time_5 = (timeout_cond+x"1")) then
            timeout_5s <= '0';
            timeout_cond <= GLOBAL_TIME(20 downto 11) + x"4";
       else
            timeout_5s \le '1';
       end if;
```

```
76
```

end if; end process;

end behaviour;

Appendix B:

Data_sender

-- data_sender.vhd

library IEEE;

use IEEE.STD_LOGIC_1164.all; use IEEE.STD_LOGIC_UNSIGNED.ALL;

entity data_sender is

PORT (

M_TIME_0	: IN std_logic;
M_TIME_6_0	: IN STD_LOGIC_VECTOR(6 DOWNTO 0);
CLK	: IN std_logic;
RESET	: IN std_logic;
H_ADC_RE	: IN std_logic; Housekeeping ADC
H_ADC_Data	: IN std_logic_vector (7 downto 0); Housekeeping ADC
Gyro_RE	: IN std_logic;
Gyro_Data	: IN std_logic_vector (7 downto 0);
E_ADC_RE	: IN std_logic; Ejection ADC
E_ADC_Data	: IN std_logic_vector (7 downto 0); Ejection ADC
Exp_Data	: OUT std_logic_vector (7 downto 0);
Exp_Data_WE	: OUT std_logic
``````````````````````````````````````	

);

end data_sender;

architecture behaviour of data_sender is

signal ADC_E_packed	: std_logic_vector (63 downto 0);
signal ADC_H_packed	: std_logic_vector (63 downto 0);
signal Gyro_packed	: std_logic_vector (63 downto 0);
signal mixed_data	: std_logic_vector (47 downto 0);
signal ADC_H_temp	: std_logic_vector (23 downto 0);
signal Gyro_temp	: std_logic_vector (23 downto 0);
signal ADC_E_temp	: std_logic_vector (35 downto 0);
signal cnt	: std_logic ;
signal cnt_old	: std_logic;

signal re	: std_logic;
signal Exp_Data_WE_int	: std_logic;

begin

```
Exp_Data_WE <= Exp_Data_WE_int;</pre>
```

```
ADC_E_Packer:process(M_TIME_0, RESET)

begin

if RESET='1' then

ADC_E_packed <= (others => '0');

elsif rising_edge(M_TIME_0) AND E_ADC_RE='1' then

if E_ADC_RE='1' then

ADC_E_packed <= ADC_E_packed(55 downto 0) & E_ADC_Data;

end if;

end if;
```

end process;

```
ADC_H_Packer:process(M_TIME_0, RESET)
```

begin

```
Gyro_Packer:process(M_TIME_0, RESET)

begin

if RESET='1' then

Gyro_packed <= (others => '0');

elsif rising_edge(M_TIME_0) AND Gyro_RE='1' then

if Gyro_RE='1' then

Gyro_packed <= Gyro_packed(55 downto 0) & Gyro_Data;
```

end if;

end if;

end process;

```
H_ADC_handling: process(M_TIME_0, RESET)

begin

if RESET = '1' then

ADC_H_temp <= (others => '0');

elsif rising_edge (M_TIME_0) AND H_ADC_RE = '0' then

if ADC_H_packed (63 downto 48) = x"01AD" then

ADC_H_temp (23 downto 12) <= ADC_H_packed (47 downto 36);

elsif ADC_H_packed (63 downto 48) = x"03AD" then

ADC_H_temp (11 downto 0) <= ADC_H_packed (11 downto 0);

end if;

end if;

end process;

gyro_handling:process (CLK, RESET)

begin

if RESET = '1' then
```

```
Gyro_temp <= (others => '0');
elsif rising_edge (CLK) AND Gyro_RE = '0' then
if Gyro_packed(63 downto 56) = x"0C" then
Gyro_temp(23 downto 16) <= Gyro_packed (55 downto 48);
Gyro_temp(15 downto 0) <= Gyro_packed (15 downto 0);
end if;
```

end if;

end process;

```
E_ADC_handling:process (CLK, RESET)

begin

if RESET = '1' then

ADC_E_temp <= (others => '0');

elsif rising_edge (CLK) AND E_ADC_RE = '0' then

if ADC_E_packed(63 downto 48) = x"01AD" then
```

```
ADC_E_temp <= ADC_E_packed (35 downto 0);
```

end if;

end if;

end process;

```
output_vector: process (CLK, RESET)
begin
 if RESET = '1' then
 mixed_data \leq (others \Rightarrow '0');
 cnt <= '0';
 re <= '0';
 cnt_old <= '0';
 elsif rising_edge(CLK) then
 re <= Exp_Data_WE_int;
 if ((re = '1' and Exp_Data_WE_int = '0')) then
 if cnt = '0' then
 mixed_data <= ADC_H_temp & Gyro_temp;</pre>
 cnt <= '1';
```

else

mixed_data <= x"000" & ADC_E_temp; cnt <= '0';

end if;

end if;

end if;

end process;

begin

WE:process (M_TIME_6_0(4), RESET) if RESET = '1' then Exp_Data_WE_int <= '0';</pre>  $elsif rising_edge(M_TIME_6_0(4))$  then if  $M_TIME_6_0(6 \text{ downto } 5) = "10"$  then Exp_Data_WE_int <= '1';</pre> else

#### Exp_Data_WE_int <= '0';</pre>

end if;

#### end if;

end process;

```
Exp_Data <= x"0"&"000"& cnt
 when M_TIME_6_0(3 downto 1)="000" else
 x"BE"
 when M_TIME_6_0(3 downto 1)="001" else
 mixed_data(47 downto 40)
 mixed_data(39 downto 32)
 mixed_data(31 downto 24)
```

mixed_data(23 downto 16) mixed_data(15 downto 8)

mixed_data(7 downto 0);

when M_TIME_6_0(3 downto 1)="010" else when M_TIME_6_0(3 downto 1)="011" else when M_TIME_6_0(3 downto 1)="100" else when M_TIME_6_0(3 downto 1)="101" else when M_TIME_6_0(3 downto 1)="110" else

end behaviour;

# Appendix C: FFU Comm switches

-- ffu_mux_rx.vhd

library IEEE; use IEEE.STD_LOGIC_1164.all; use IEEE.STD_LOGIC_UNSIGNED.ALL;

```
entity ffu_mux_rx is
PORT (
 MUX
 : in std_logic_vector (1 downto 0);
 serial_out : in std_logic;
 : out std_logic;
 RXSU_RX
 RXCU_RX
 : out std_logic;
 TXCU_RX
 : out std_logic
);
end ffu_mux_rx;
ARCHITECTURE mux OF ffu_mux_rx IS
begin
process (serial_out,MUX)
begin
case MUX is
 when "01" => TXCU_RX <= serial_out;
 when "10" => RXCU_RX <= serial_out;
 when "11" => RXSU_RX <= serial_out;
```

when others => null;

end case;

end process;

```
end mux;
```

-- ffu_mux_tx.vhd

library IEEE;

use IEEE.STD_LOGIC_1164.all; use IEEE.STD_LOGIC_UNSIGNED.ALL;

end ffu_mux_tx;

```
ARCHITECTURE mux OF ffu_mux_tx IS
begin
RX_out <= TXCU_RX_in when MUX = "01" else
RXCU_RX_in when MUX = "10" else
RXSU_RX_in when MUX = "11" else
'1';
end mux;
```

## **Appendix D:**

### **RxSU** Comm switch

-- switch2.vhd

library IEEE; use IEEE.std_logic_1164.all; use IEEE.std_logic_unsigned.all; use IEEE.numeric_std.all;

entity switch2 is

Port(

:in std logic; TX_MAIN UART_CAM_TX : in std_logic; UART_SF2_TX : in std_logic; UART_IR_TX : :in std_logic; UART_SENS_RX : in std_logic; :in std_logic_vector(1 downto 0); switch RX MAIN :out std_logic; UART_CAM_RX :out std_logic; UART_SENS_TX :out std_logic; UART_IR_RX :out std_logic; UART_SF2_RX :out std_logic ); end switch2:

architecture behavioral of switch2 is begin

RX_MAIN <= UART_SENS_RX;

```
mux : process (TX_MAIN,UART_CAM_TX,UART_SF2_TX,UART_SENS_RX,switch)
begin
 case switch is
 when "00" =>
 UART_SENS_TX <= TX_MAIN;
 UART_CAM_RX <= '1';
 UART_SF2_RX <= '1';
 UART_IR_RX <= '1';
 when "01" =>
 UART_CAM_RX <= UART_SENS_RX;
 UART_SENS_TX <= UART_CAM_TX;
 UART_SF2_RX <= '1';
 UART_IR_RX <= '1';
 when "10" =>
 UART_SF2_RX <= UART_SENS_RX;
 UART_SENS_TX <= UART_SF2_TX;
 UART_CAM_RX <= '1';
 UART_IR_RX <= '1';
 when "11" =>
 UART_IR_RX <= UART_SENS_RX;
```

UART_SENS_TX <= UART_IR_TX; UART_CAM_RX <= '1'; UART_SF2_RX <= '1'; when others => null; end case; end process;

end behavioral;

```
-- CommuCon.vhd
library IEEE;
use IEEE.std_logic_1164.all;
use ieee.std_logic_unsigned.all;
use IEEE.numeric std.all;
entity CommuCon is
port (
 CLK
 : in std_logic;
 RESET
 : in std_logic;
 : in std_logic_vector(7 downto 0);
 RX BYTE
 RX_BYTE_OK : in std_logic;
 : out std_logic_vector (1 downto 0)
 switch
);
end CommuCon;
architecture behavioral of CommuCon is
 signal rxByte : std_logic_vector(7 downto 0);
 signal rxBit0 : std_logic;
signal rxBit1 : std_logic;
 signal rx_state : std_logic;
 signal switch_int : std_logic_vector (1 downto 0);
begin
 switch <= switch_int;</pre>
 process (CLK, RESET)
 begin
 if RESET = '1' then
 rx_state \leq 0';
 rxByte \langle = (others = \rangle '0');
 rxBit0 <= '0';
 rxBit1 <= '0';
 switch_int <= "10";</pre>
 elsif rising_edge(CLK) then
 rxBit0 <= RX_BYTE_OK;
 rxBit1 <= rxBit0;
 if rx_state = '0' then
 if rxBit0 = '1' and rxBit1 = '0' then
 rxByte <= RX_BYTE;
 rx state \leq 1':
 else
 rx_state <= '0';
 end if;
 else
 rx_state <= '0';
 case rxByte is
 when x"25" => switch_int <= "00"; -- % for sensor FPGA
 when x"26" => switch_int <= "01"; -- & for camera FPGA
 when x"28" => switch_int <= "10"; -- (for SmartFusion2
 when x''29'' \Rightarrow switch int \langle = "00"; -- \rangle for IR FPGA
 when others => null;
 end case;
 end if;
 end if:
end process;
end behavioral;
```